

Appendix H

Derivation of the Scattered Fields

in the Medium 2 at Burnt Coal Seam and Peat Interface

From (5.45), the vector nature of ${}^o E^s$ is characterized by

$$\begin{aligned} {}^o E_n^s &\equiv E^s / KI_1 \\ &= \hat{\mathbf{n}}_{so}^t \times (\hat{\mathbf{n}}_2 \times \mathbf{E} - \hat{\mathbf{n}}_{so}^t \times (\mathbf{h}_2 \hat{\mathbf{n}}_1 \times \mathbf{H})) \\ &= \hat{\mathbf{n}}_{so}^t \times (\hat{\mathbf{n}}_2 \times \mathbf{E}) + (\mathbf{h}_2 \hat{\mathbf{n}}_2 \times \mathbf{H}) - (\hat{\mathbf{n}}_{so}^t \cdot (\mathbf{h}_2 \hat{\mathbf{n}}_2 \times \mathbf{H})) \hat{\mathbf{n}}_{so}^t \end{aligned} \quad (\text{H.1})$$

The polarization factors are

$$\hat{\mathbf{h}}_{so} \cdot {}^o E_n^s = \hat{\mathbf{v}}_{so} \cdot (\hat{\mathbf{n}}_2 \times \mathbf{E}) + \hat{\mathbf{h}}_{so} \cdot (\mathbf{h}_2 \hat{\mathbf{n}}_2 \times \mathbf{H}) \quad (\text{H.2})$$

$$\hat{\mathbf{v}}_{so} \cdot {}^o E_n^s = -\hat{\mathbf{h}}_{so} \cdot (\hat{\mathbf{n}}_2 \times \mathbf{E}) + \hat{\mathbf{v}}_{so} \cdot (\mathbf{h}_2 \hat{\mathbf{n}}_2 \times \mathbf{H}) \quad (\text{H.3})$$

Under the stationary-phase approximation, $\hat{\mathbf{n}}_1$, $\hat{\mathbf{t}}$, $\hat{\mathbf{d}}$ can be expressed in terms of propagation vectors, $\hat{\mathbf{n}}_{so}$ and $\hat{\mathbf{n}}_i$, as in Appendix G.

$$\hat{\mathbf{n}}_1 = \frac{(\hat{x}\bar{q}_x + \hat{y}\bar{q}_y + \hat{z}\bar{q}_z)|\bar{q}_z|}{\bar{q}_z\bar{q}} = \frac{(k_2\hat{\mathbf{n}}_{so} - k_1\hat{\mathbf{n}}_i)|\bar{q}_z|}{\bar{q}_z\bar{q}} \quad (\text{H.4})$$

where

$$\bar{q}^2 = \bar{q}_x^2 + \bar{q}_y^2 + \bar{q}_z^2 = k_1^2 + k_2^2 - 2k_1k_2(\hat{\mathbf{n}}_{so} \cdot \hat{\mathbf{n}}_i) \quad (\text{H.5})$$

$$\hat{\mathbf{t}} = \frac{(\hat{\mathbf{n}}_1 \times \hat{\mathbf{n}}_{so})|q_z|}{\bar{q}_z D_2} \quad (\text{H.6})$$

$$D_2 = |\hat{\mathbf{n}}_i \times \hat{\mathbf{n}}_{so}| = |\hat{\mathbf{n}}_i \times (\hat{\mathbf{h}}_{so} \times \hat{\mathbf{v}}_{so})| = \left| (\hat{\mathbf{n}}_i \cdot \hat{\mathbf{v}}_{so})^2 + (\hat{\mathbf{n}}_i \cdot \hat{\mathbf{h}}_{so})^2 \right|^{\frac{1}{2}} \quad (\text{H.7})$$

$$\hat{\mathbf{d}} = \hat{\mathbf{n}}_i \times \hat{\mathbf{t}} = ((\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so})\hat{\mathbf{n}}_i - \hat{\mathbf{n}}_{so})|\bar{q}_z| / (\bar{q}_z D_2) \quad (\text{H.8})$$

with these local coordinate vectors expressed in $\hat{\mathbf{n}}_i$ and $\hat{\mathbf{n}}_{so}$, all other vector products can be

expressed in $\hat{\mathbf{n}}_i$ and $\hat{\mathbf{n}}_{so}$

$$\hat{\mathbf{n}}_2 \times \hat{\mathbf{t}} = \frac{\{k_1(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so}) - k_2\}\hat{\mathbf{n}}_i + \{k_2(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so}) - k_1\}\hat{\mathbf{n}}_{so}}{\bar{q}D_2} \quad (\text{H.9})$$

$$\hat{\mathbf{n}}_2 \cdot \hat{\mathbf{n}}_{so} = -(k_2 - k_1(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so}))\bar{q}_z / |\bar{q}\bar{q}_z| = \hat{\mathbf{n}}_2 \cdot \hat{\mathbf{n}}_t \equiv \cos \mathbf{F}_o \quad (\text{H.10})$$

$$\hat{\mathbf{h}} \cdot \hat{\mathbf{t}} = (\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so}) / \bar{D}_2 \quad (\text{H.11})$$

$$\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{t}} = -(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i) / \bar{D}_2 \quad (\text{H.12})$$

$$\hat{\mathbf{v}} \cdot \hat{\mathbf{t}} = -(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so}) / \bar{D}_2 \quad (\text{H.13})$$

$$\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{t}} = -(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i) / \bar{D}_2 \quad (\text{H.14})$$

$$\hat{\mathbf{h}} \cdot \hat{\mathbf{d}} = -(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so}) / \bar{D}_2 \quad (\text{H.15})$$

$$\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{d}} = (\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i) / \bar{D}_2 \quad (\text{H.16})$$

$$\hat{\mathbf{v}} \cdot \hat{\mathbf{d}} = -(\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so}) / \bar{D}_2 \quad (\text{H.17})$$

$$\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{d}} = (\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i) / \bar{D}_2 \quad (\text{H.18})$$

where

$$D_2 = \bar{q}_z D_2 / |\bar{q}_z| \quad (\text{H.19})$$

$$\hat{\mathbf{v}}_{so} \cdot (\hat{\mathbf{n}}_2 \times \hat{\mathbf{t}}) = (\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i)(k_1(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so}) - k_2) / (\bar{q}D_2) \quad (\text{H.20})$$

$$\hat{\mathbf{h}}_{so} \cdot (\hat{\mathbf{n}}_2 \times \hat{\mathbf{t}}) = (\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i)(k_1(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so}) - k_2) / (\bar{q}D_1) \quad (\text{H.21})$$

with the above vector identities (H.2) and (H.3) can be expressed in $\hat{\mathbf{n}}_i$ and $\hat{\mathbf{n}}_{so}$. For

horizontally polarized incident wave

$$\begin{aligned}
\hat{\mathbf{v}}_{so} \cdot (\hat{\mathbf{n}}_2 \times \mathbf{E}) &= (T_{\perp}(\hat{\mathbf{h}} \cdot \hat{\mathbf{t}})(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_2 \times \hat{\mathbf{t}}) - T_{\parallel}(\hat{\mathbf{h}} \cdot \hat{\mathbf{d}})(\hat{\mathbf{n}}_2 \cdot \hat{\mathbf{n}}_t)(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{t}})\mathbf{h}_2/\mathbf{h}_1)E_o \\
&= -\{k_2 - k_1(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so})\}E_o \times \frac{T_{\perp}(\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i) + T_{\parallel}(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i)\mathbf{h}_2/\mathbf{h}_1}{\bar{q}D_2\bar{D}_2}
\end{aligned} \tag{H.22}$$

$$\begin{aligned}
\hat{\mathbf{h}}_{so} \cdot (\mathbf{h}_2 \hat{\mathbf{n}}_2 \times \mathbf{H}) &= -(T_{\perp}(\hat{\mathbf{h}} \cdot \hat{\mathbf{t}})(\hat{\mathbf{n}}_1 \cdot \hat{\mathbf{n}}_t)(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{t}}) + T_{\parallel}(\hat{\mathbf{h}} \cdot \hat{\mathbf{d}})(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_2 \times \hat{\mathbf{t}})\mathbf{h}_2/\mathbf{h}_1)E_o \\
&= (\text{H.22})
\end{aligned} \tag{H.23}$$

$$\begin{aligned}
\hat{\mathbf{v}}_{so} \cdot (\mathbf{h}_2 \hat{\mathbf{n}}_2 \times \mathbf{H}) &= -(T_{\perp}(\hat{\mathbf{h}} \cdot \hat{\mathbf{t}})(\hat{\mathbf{n}}_2 \cdot \hat{\mathbf{n}}_t)(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{t}}) + T_{\parallel}(\hat{\mathbf{h}} \cdot \hat{\mathbf{d}})(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_2 \times \hat{\mathbf{t}})\mathbf{h}_2/\mathbf{h}_1)E_o \\
&= \{k_2 - k_1(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so})\}E_o \times \frac{T_{\perp}(\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i) - T_{\parallel}(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i)\mathbf{h}_2/\mathbf{h}_1}{\bar{q}D_2\bar{D}_2}
\end{aligned} \tag{H.24}$$

$$\begin{aligned}
\hat{\mathbf{h}}_{so} \cdot (\hat{\mathbf{n}}_2 \times \mathbf{E}) &= (T_{\perp}(\hat{\mathbf{h}} \cdot \hat{\mathbf{t}})(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_2 \times \hat{\mathbf{t}}) - T_{\parallel}(\hat{\mathbf{h}} \cdot \hat{\mathbf{d}})(\hat{\mathbf{n}}_2 \cdot \hat{\mathbf{n}}_t)(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{t}})\mathbf{h}_2/\mathbf{h}_1)E_o \\
&= -(\text{H.24})
\end{aligned} \tag{H.25}$$

By substituting (H.22) through (H.25) into (H.2) and (H.3), we obtain

$$\begin{aligned}
{}^o E_{hh}^s &= KI_2(\hat{\mathbf{h}}_{so} \cdot {}^o \mathbf{E}_n^s) \\
&= -M_2 \{T_{\perp}(\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i) + T_{\parallel}(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so})(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i)\mathbf{h}_2/\mathbf{h}_1\}
\end{aligned} \tag{H.26}$$

$$\begin{aligned}
{}^o E_{vh}^s &= KI_2(\hat{\mathbf{v}}_{so} \cdot {}^o \mathbf{E}_n^s) \\
&= M_2 \{T_{\perp}(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i)(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so}) - T_{\parallel}(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i)(\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so})\mathbf{h}_2/\mathbf{h}_1\}
\end{aligned} \tag{H.27}$$

where $M_2 = 2KI_2E_o(k_2 - k_1(\hat{\mathbf{n}}_i \cdot \hat{\mathbf{n}}_{so})) / (\bar{q}D_2\bar{D}_2)$. For a vertically polarized incident wave,

${}^o E_{vv}^s$ and ${}^o E_{hv}^s$ can be obtained from (H.26) and (H.27) respectively by interchanging $\hat{\mathbf{v}}$

with $\hat{\mathbf{h}}$, and $\hat{\mathbf{v}}_{so}$ with $\hat{\mathbf{h}}_{so}$

$${}^o E_{vv}^s = -M_2 \{T_{\perp}(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i)(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so}) + T_{\parallel}(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i)(\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so})\mathbf{h}_2/\mathbf{h}_1\} \tag{H.28}$$

$${}^o E_{hv}^s = M_2 \{T_{\perp}(\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i)(\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so}) - T_{\parallel}(\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i)(\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so})\mathbf{h}_2/\mathbf{h}_1\} \tag{H.29}$$

The dot products in the field expressions are given by

$$\hat{\mathbf{v}}_{so} \cdot \hat{\mathbf{n}}_i = -\sin \mathbf{q}_o \cos \mathbf{q}_{so}^t \cos(\mathbf{f}_{so} - \mathbf{f}_o) + \cos \mathbf{q}_o \sin \mathbf{q}_{so}^t \tag{H.30}$$

$$\hat{\mathbf{v}} \cdot \hat{\mathbf{n}}_{so} = -\cos \mathbf{q}_o \sin \mathbf{q}_{so}^t \cos(\mathbf{f}_{so} - \mathbf{f}_o) + \sin \mathbf{q}_o \cos \mathbf{q}_{so}^t \tag{H.31}$$

$$\hat{\mathbf{h}}_{so} \cdot \hat{\mathbf{n}}_i = -\sin \mathbf{q}_o \sin(\mathbf{f}_{so} - \mathbf{f}_o) \quad (\text{H.32})$$

$$\hat{\mathbf{h}} \cdot \hat{\mathbf{n}}_{so} = \sin \mathbf{q}_{so}^t \sin(\mathbf{f}_{so} - \mathbf{f}_o) \quad (\text{H.33})$$